All-Solution-Processed, Oxidation-Resistant Copper Nanowire Networks for Optoelectronic Applications with Year-Long Stability

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ABSTRACT: Copper nanowires (Cu NWs) hold promise as they possess equivalent intrinsic electrical conductivity and optical transparency to silver nanowires (Ag NWs) and cost substantially less. However, poor resistance to oxidation is the historical challenge that has prevented the large-scale industrial utilization of Cu NWs. Here, we use benzotriazole (BTA), an organic corrosion inhibitor, to passivate Cu NW networks. The stability of BTA-passivated networks under various environmental conditions was monitored and compared to that of bare Cu NW control samples. BTA passivation greatly enhanced the stability of networks without deteriorating their optoelectronic performance. Moreover, to demonstrate their potential, BTA-passivated networks were successfully utilized in the fabrication of a flexible capacitive tactile sensor. This passivation strategy has a strong potential to pave the way for large-scale utilization of Cu NW networks in optoelectronic devices.

KEYWORDS: copper nanowires, benzotriazole, oxidation stability, passivation, transparent conducting electrodes, flexible tactile sensors

INTRODUCTION

Transparent electrodes are key components of many optoelectronic devices such as touch panels, photovoltaic devices, light-emitting diodes, and transparent thin-film heaters.1,2 Although the majority of commercial products in the market are based on indium tin oxide (ITO) thin films, high processing costs, brittleness, and indium scarcity renders ITO-based systems undesirable in the next generation of optoelectronic devices requiring mechanical and functional flexibility. Therefore, much effort has been devoted to the development of mechanically flexible, large-scale processable, low-cost, and lightweight alternative materials for transparent and conducting electrodes. Ag NW networks appear to be the most promising alternative due to their equivalent or better optoelectronic performance than that of ITO.3–6 Cu NWs also hold great potential because they possess comparable intrinsic electrical conductivity to Ag NWs ($\rho_{\text{Ag}} = 1.6 \times 10^{-8}$ $\Omega$ m, $\rho_{\text{Cu}} = 1.7 \times 10^{-8}$ $\Omega$ m) and are lower in cost.7 Successful integration of Cu NW networks as transparent conducting electrodes into a variety of functional prototype devices, such as organic photovoltaics,8–10 organic light-emitting diodes11–13 touch sensors,14,15 and transparent thin-film heaters,16–18 has already been demonstrated. However, poor oxidation stability of Cu NWs presents a major barrier in front of their utilization in mass-produced commercial devices. Therefore, the development of an efficient method to protect Cu NW networks from atmospheric corrosion without deteriorating their optoelectronic performance is a crucial challenge of paramount significance. Various routes have been proposed to solve the stability issue. These include coating Cu NWs with metals,7,18–20 metal oxides,9,16,21,22 carbon, nitride-based materials23–25 and polymers.10,26 Despite these studies, development of Cu NW-based network fabrication routes that can (i) enable highly efficient long-term corrosion protection, (ii) preserve the optoelectronic performance of the network (particularly sheet resistance, transmittance, and haze), and (iii) allow quick, affordable, and simple means of mass production of large-area electrodes remain elusive.

It is well known that bulk Cu is prone to oxidation. Thus, numerous methods have been proposed to increase its oxidation stability. For instance, studies have reported the use of organic corrosion inhibitors (e.g., azoles, amines, amino acids, self-assembled monolayers) that are effective in enhancing oxidation resistance of bulk copper.27–29 Among these, azoles such as benzotriazole (BTA), benzimidazoles,
tetrazole, pyridazole, other nitrogen-containing heterocyclic compounds, and their derivatives have been demonstrated as highly efficient corrosion inhibitors for bulk Cu and its alloys. In particular, outstanding corrosion inhibition efficiency for bulk Cu was reported using BTA. The stabilization of Cu using BTA has been ascribed to the formation of a polymeric barrier film that is insoluble in water and many organic solvents.\(^1\)\(^2\)\(^3\)\(^4\)\(^5\) BTA was also used for improving the stability of Cu nanoparticles\(^33\) and Cu NWs.\(^34\) Wiley’s group demonstrated the first use of BTA for improving the stability of Cu NW networks and their consequent use as transparent electrodes in organic photovoltaic devices.\(^34\) However, a 20% increase in the sheet resistance of Cu NW networks was reported upon BTA deposition, probably due to the use of the aqueous soaking solution for BTA deposition.\(^34\)

In the current study, BTA was utilized to enhance the long-term oxidation stability of Cu NW networks without degrading their performance. High-aspect-ratio Cu NWs synthesized through a hydrothermal method were used to deposit optically transparent and electrically conducting Cu NW networks. Optoelectronic properties of Cu NW networks under ambient conditions as well as under operationally harsh environments were systemically investigated and compared to that of bare Cu NW control samples. A clear understanding of the limits of BTA passivation on Cu NW networks through detailed spectroscopic and structural analysis was provided. At last, BTA-passivated networks were successfully utilized in transparent and flexible capacitive tactile sensors that can be integrated into a variety of devices.

**RESULTS AND DISCUSSION**

Following the synthesis of Cu NWs through a hydrothermal method, Cu NW networks were fabricated via a simple spray deposition method. Figure 1a schematically illustrates the fabrication process of transparent and conducting Cu NW networks. Note that this simple yet effective production method can readily be utilized to manufacture large-scale electrodes with high speed, high quality, and low production cost. Furthermore, this deposition method is substrate-neutral as it can be used to coat any substrate. Following fabrication, Cu NW networks were passivated with BTA that was practiced through spin coating of a 3 wt % BTA—ethanol solution, followed by an ethanol rinse and drying.

To investigate the stability of Cu NW-based electrodes, it is crucial to elucidate the structural and functional characteristics of individual NWs as well as the entire NW networks. The average diameter and length of synthesized Cu NWs were 45.4 ± 17.4 nm and 49.3 ± 19.9 μm, respectively (Figure S1). Prior to annealing, all bare Cu NW networks were found to be nearly insulating with sheet resistance values on the order of 10\(^6\) Ω/sq with optical transmittance values higher than 70% (at 550 nm). Annealing was performed to remove the residual surfactant (PVP) layer and the residual capping agent (HDA) and to improve the electrical contacts by fusing nanowire—nanowire junctions. After annealing, the typical sheet resistance of bare Cu NW networks was found to be 30 ± 9 Ω/sq at an optical transmittance (at 550 nm) of 86%. The sheet resistance and transmittance values of networks can be simply controlled with NW density. The change in sheet resistance with the optical transmittance of Cu NW networks both before and after BTA passivation in comparison to several other studies in the literature on transparent electrodes is provided in Figure 1b. BTA passivation resulted in a minute increase in sheet resistance (of 1 Ω/sq) and a slight decrease in optical transmittance (of 2%). Hence, no significant changes were detected due to the passivation process and BTA-passivated networks showed comparable figure-of-merit transparency and sheet resistance to those of bare Cu NW networks (Figure 1b).

X-ray photoelectron spectroscopy (XPS) analysis was performed to determine the initial compositions of the as-prepared and BTA-passivated networks. It was found that the as-deposited bare Cu NW networks were mostly in the oxidic form (i.e., predominantly CuO with a minor contribution from Cu\(_2\)O) evident by the appearance of a high Cu 2p\(_{3/2}\) binding energy (B.E.) shoulder at 934.0 eV as well as the strong satellite peak at ca. 944 eV (Figure S2a). Obviously, without BTA protection, metallic Cu is not likely to survive on the surface even under ambient conditions during the short time period between network fabrication and XPS measurements. However, the high electrical conductivity of bare Cu NW networks signifies that the Cu NWs are not entirely oxidized and metallic Cu possibly resides below the CuO and Cu\(_2\)O layers on the surface. Moreover, it should be noted that the

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**Figure 1.** (a) Schematic illustration for the fabrication of transparent and conducting Cu NW networks. (b) Sheet resistance versus transmittance (at 550 nm) of Cu NW networks (before and after BTA passivation) in comparison to various transparent electrodes reported in the literature including ITO. Photographs of (c) bare and (d) BTA-passivated Cu NW networks.
presence of $\text{Cu}_2\text{O}$ on the outermost surface cannot be ruled out, as its Cu 2p signals overlap with those of Cu. Overall, the structure of fresh, bare Cu NW networks was possibly in the form of either a CuO shell with a Cu core and/or a CuO + $\text{Cu}_2\text{O}$ shell with a Cu core. In sharp contrast, it was found that there is no CuO on BTA-passivated Cu NW networks due to the absence of high B.E. Cu 2p$_{3/2}$ shoulder at 934.0 eV, and the strong satellite at 944 eV (Figure S2b). As a result, the structure of BTA-passivated Cu NW networks is possibly in the form of prominently metallic Cu with some adsorbed O (due to $\text{H}_2\text{O}$ or $-\text{OH}$) and perhaps very small amounts of $\text{Cu}_2\text{O}$.

At last, it should be noted that the stability of transparent and conducting metallic NW networks strongly depends on the amount of NWs forming the network. Although there exists a vast number of studies in the literature on the stability of metallic NW networks, most of these studies fail to report the NW density of the fabricated networks. This makes relative stability comparisons of the different types of metal NW networks difficult. In the current study, the density of Cu NW networks was calculated for each network as areal mass density (amd) in units of mg/m$^2$. The amd calculation details are provided in Supporting Information Figure S3a,b. Networks with amd values of 120–162 mg/m$^2$ were used for all stability tests reported here.

**Oxidation Resistance of Networks under Ambient Conditions.** To compare the oxidation resistance performance under ambient conditions, sheet resistances of bare Cu NW and BTA-passivated Cu NW networks were monitored for an extended period of time (i.e., 1 year). Networks were prepared with similar NW densities of 124–148 mg/m$^2$ to eliminate the effect of the NW density on the degradation of electrodes. During measurements, all electrodes were kept under atmospherically regulated conditions (i.e., in air with an average temperature of 22 ± 2 °C and average humidity of 25 ± 5% RH). The normalized sheet resistance—the ratio of the sheet resistance to the initial sheet resistance ($R/R_0$)—was used as a test standard. Figure 2a shows the graph of normalized sheet resistance versus time for bare and BTA-passivated Cu NW networks. Bare Cu NWs lost their conductivity within 12 days, while the sheet resistance of BTA-passivated networks increased by a factor of only 1.1 at the end of one year. Scanning electron microscopy (SEM) images of bare and BTA-passivated Cu NW networks after a one-year test period are shown in Figure 2b,c, respectively. The surface roughness of bare Cu NWs was found to increase dramatically. In sharp contrast, BTA-passivated Cu NWs preserved their smoothness and no prominent morphological changes were observed. XPS analysis of bare Cu NW networks upon exposure to ambient conditions during a year-long exposure to ambient conditions suggested that the loss in electrical conductivity and the change in morphology of Cu NWs were due to complete oxidation of Cu to CuO. This was evidenced by the appearance of characteristic strong satellite peaks at 943.6 and 962.0 eV (Figure S4).

**Oxidation Resistance of Networks at High Relative Humidity Conditions.** To accelerate their degradation, Cu NW electrodes were also stored under high relative humidity (RH) environments (e.g., 75 and 90% RH) for 10 days. Sheet resistance values along with the structural properties of the electrodes were monitored via conductivity measurements and XPS and transmission electron microscopy (TEM) analyses. Networks prepared for these studies had similar NW densities of 148–162 mg/m$^2$. Increased humidity severely affected the stability of bare Cu NW networks. Although bare Cu NW networks lost their electrical conductivity due to oxidation in 12 days under ambient conditions, it took approximately 5 days for the complete loss of conductivity under 75% RH (Figure 3a). The corrosion rate was much higher under 90% RH for bare Cu NW networks so that they became nonconducting only after 2 days (Figure 3a). In sharp contrast, the resistance change for BTA-passivated Cu NW networks was negligible at the end of 10 days. The chemical composition of NWs after exposure to high humidity conditions was determined through XPS analysis. Characteristic strong satellite peaks appearing at 942.5 and 962.2 eV, as well as Cu 2p$_{3/2}$ and Cu 2p$_{1/2}$ peaks at 933.3 and 953.1 eV, respectively, in the XPS spectrum revealed that the bare Cu NWs were oxidized predominantly to CuO with a minor contribution from Cu$_3$O$_2$ (Figure S5). SEM and TEM images provided in Figure 3b,c, respectively, reveal nanoparticle formation on the surface of the bare Cu NWs upon exposure to high humidity conditions. Since the polycrystalline oxide layer forms throughout the surface of NWs, the formed grain boundaries and other types of defects act as nucleation sites for the formation of CuO/Cu$_2$O nanoparticles.

**Oxidation Resistance of Networks at Elevated Temperatures.** Since typical optoelectronic device fabrication processes involve multiple annealing steps, Cu NW networks should be thermally stable at these elevated temperatures. To compare the thermal stability of bare and BTA-passivated Cu NW networks, samples were calcined at 75, 125, and 150 °C in air. The average initial sheet resistance of these Cu NW networks was 19 ± 3.8 Ω/sq, while the initial areal mass density of networks was in the range of 120–150 mg/m$^2$. For all thermal aging tests, samples were directly exposed to the chosen temperatures in air without a heating ramp. Figure 3d–f shows the change in the sheet resistance for both bare and BTA-passivated Cu NW networks as a function of the time at calcination temperatures of 75, 125, and 150 °C, respectively. At 75 °C, BTA-passivated networks showed superior stability with respect to the bare networks (Figure 3d). Although it took approximately 250 min for the bare Cu NW network to be totally nonconductive at 75 °C, similar failure occurred within 50 min at 125 °C and only within 20 min at 150 °C. On the other hand, BTA-passivated Cu NW networks showed better resistance against oxidation compared to the bare Cu
NW samples (Figure 3e,f). Typical annealing temperatures involved in the fabrication of optoelectronic devices lie around 100 °C, and hence, BTA-passivated Cu NW networks will survive these processes. Moreover, the rate of change in resistance values decreased significantly before networks became completely insulating for all of the calcination temperatures investigated (Figure 3d–f). This very slow rate could be attributed to the gradual loss of BTA following the rapid loss at the initial stage.37

To determine the oxidation states of both bare and BTA-passivated Cu NW networks, XPS analysis was performed following 5 min calcination at 75, 125, and 150 °C. Three major factors may tend to change the oxidation state of Cu in the presence of atmospheric oxygen and thermal activation provided by calcination/heat. Firstly, atmospheric O₂ can be activated and dissociated on the Cu surface, leading to the oxidation of Cu. This was observed for the freshly prepared bare Cu NW networks at 25 °C (Figure 4b), where the surface of the Cu NWs was determined to be oxidized to predominantly Cu²⁺ (i.e., CuO) species with a smaller contribution from Cu¹⁺ (i.e., Cu₂O) species. Oxidation of metallic Cu to Cu²⁺ and Cu¹⁺ is clearly discernible by the
presence of the satellite features in Figure 4b, as well as the high B.E. shoulder at 934.0 eV in the Cu 2p$_{3/2}$ signal (Figure 4c). The second factor influencing the Cu oxidation state during the thermal treatment can be the desorption/loss of lattice oxygen from CuO and Cu$_2$O structures. In contrast to the first factor, this second factor tends to reduce Cu$^{2+}$ to Cu$^+$ and—less likely—Cu$^+$ to Cu species. Finally, as the third factor, oxidation of the surface C and N residues originating from hexadecylamine (HDA) and poly(vinylpyrrolidone) (PVP) used in the synthesis and incorporation of CuO and Cu$_2$O lattice oxygen to the surface organic functionalities may also tend to reduce CuO to Cu$_2$O and less likely Cu$_2$O to Cu. Hence, there are multiple opposing processes favoring oxidation or reduction of the Cu NW surface upon calcination in air. This is also apparent in the oscillatory behavior of the oxidation state of the bare Cu NWs upon calcination in air, where at 25 °C, the bare Cu NW surface is dominated by CuO with a minor contribution from Cu$_2$O (note the minor 945.1 eV Cu$_2$O satellite feature at 25 °C). However, upon calcination at 75 °C, a partial reduction was observed and bare Cu NWs tend to reveal mostly Cu$_2$O species, evident by the loss of the high B.E. Cu 2p$_{3/2}$ shoulder at 934.0 eV, sharpening of the Cu 2p$_{3/2}$ signal, a decrease in the 943.3 eV CuO satellite feature, and strengthening of the 946.1 eV Cu$_2$O satellite feature (Figure 4b). Upon calcination at a higher temperature of 125 °C, Cu$_2$O was reoxidized to CuO, which was readily visible through the reappearance of the 934.0 eV Cu 2p$_{3/2}$ shoulder and 943.3 eV satellite feature. Further calcination at 150 °C tended to partially reduce the Cu NWs back to mostly Cu$_2$O (see the satellite in Figure 4b). These oxidation state variations of bare Cu NW network as a function of temperature was also in accordance with the surface atomic oxygen content determined via XPS measurements (see Figure S6a).

When Cu NWs were passivated with BTA, Cu sites tend to protect their metallic nature in air for all investigated temperatures (25–150 °C) (Figure 4a–c). The lack of a significant amount of CuO was evident due to the Cu 2p$_{3/2}$ B.E. located at 931.9 eV and the absence of a high B.E. shoulder at 934.0 eV. The presence of a significant amount of Cu$_2$O could also be readily ruled out by considering the lack of a satellite peak at 944 eV and more importantly by considering the minuscule concentration of surface atomic oxygen (ca. 2%) determined by XPS (Figure S6b). It is obvious that BTA provided an excellent oxidation resistance for metallic Cu sites within 25–150 °C in air for moderate time periods.

To demonstrate the thermal stability of BTA on Cu NW networks, passivated networks were monitored through ATR-IR spectroscopy upon 5 min calcination within a temperature range of 25–250 °C. Figure 4d shows that the BTA overlayer remains intact after calcination in air up to 125 °C, while it drastically decomposes after calcination at 150 °C.

Detailed ATR data for the BTA-passivated Cu NW networks calcined at 25 °C (black spectrum in Figure 4e) are in very good agreement with the former studies. It was apparent that after calcination at 150 °C, most of the vibrational features either disappear completely or significantly attenuate in intensity. ATR-IR spectra after calcination within 150–250 °C were almost identical, suggesting that following the drastic transformation at T ≥ 150 °C, the vibrational structure was starkly modified, but this modified structure remained rather intact at temperatures above 150 °C. The ATR-IR spectrum obtained after calcination at 250 °C (red spectrum in Figure 4e) revealed two major modes that can survive upon calcination at temperatures above 150 °C, a $\gamma_{C-H}$ (out-of-plane bending/obp) mode at 735 cm$^{-1}$ and a $\delta_{C-H}$ (in-plane bending/ibp) mode at 1149 cm$^{-1}$. These features indicate the presence of an aromatic organic coating on Cu NWs following the degradation of the BTA overlayer. Furthermore, bare Cu NWs (blue spectrum in Figure 4e) have IR features at 661 and 647 cm$^{-1}$, which can be associated with copper oxide phonon modes in line with the current XPS results (see XPS data for bare Cu NWs in Figure 4b). Therefore, the absence of such phonon modes for BTA-passivated Cu NW networks in Figure 4e suggests that BTA covers the Cu NW networks effectively without leaving a significant amount of uncovered/bare Cu NWs.

**Chemical Corrosion Stability of Networks under the PEDOT:PSS Layer.** Either as a hole injection or a hole transparent layer, transport electrodes are generally in contact with a PEDOT:PSS layer in organic-based optoelectronic devices. Most of the PEDOT:PSS types used in optoelectronic devices have relatively high acidity (pH ~ 3–4). Thus, the acidic nature of PEDOT:PSS eventually deteriorates the NW networks by acidic corrosion. As a result, long-term chemical corrosion stability against the acidic nature of PEDOT:PSS is another crucial requirement in industrial applications of transparent conducting electrodes. In this study, bare and BTA-passivated Cu NW networks were spin-coated with a 50 nm thick PEDOT:PSS (pH ~ 3) layer. Then, the stability of both bare Cu NW/PEDOT:PSS and Cu NW/BTA/PEDOT:PSS samples was monitored through sheet resistance measurements for 4 months. PEDOT:PSS is well known to be sensitive to air exposure, and its electrical conductivity degrades in time due to the absorption of atmospheric water/oxygen. Therefore, all samples were kept in a glovebox under a controlled argon atmosphere (O$_2$ level <0.1 ppm, H$_2$O level <0.1 ppm) throughout the test period to assure that the change in resistance was not related to the degradation of PEDOT:PSS. The initial average resistances for Cu NW/PEDOT:PSS samples and Cu NW/BTA/PEDOT:PSS samples were measured as 27 ± 4 and 25 ± 2, respectively. At the end of 4 months, the resistance of Cu NW/PEDOT:PSS samples increased by approximately 500 times, while the resistance of Cu NW/BTA/PEDOT:PSS samples increased by only 5 times (Figure 5a). It should also be noted that the maximum resistance of Cu NW/BTA/PEDOT:PSS samples at the end of 4 months was below 150
$\Omega/$sq, which is still low enough for many optoelectronic applications. The obtained results were also supported by SEM analysis. The SEM image of the bare Cu NW/PEDOT:PSS sample showed that the structural integrity of the network was lost due to severe etching of the NWs (Figure 5b). Due to the acidic nature of PEDOT:PSS, bare Cu NWs were dissolved and ruptured within this acidic polymeric media. The overall electrical percolation within the network was destroyed, confirming the sheet resistance measurements. On the other hand, no morphological changes were observed for the Cu NW/BTA/PEDOT:PSS samples (Figure 5c). This implies that BTA-passivated samples show superior resistance against corrosion. The BTA layer deposited by a simple, solution-based method suppresses the corrosion rate of Cu NWs under acidic conditions. These results are in perfect agreement with previous studies, where BTA treatment was shown to decrease the acidic corrosion rate of bulk Cu.43

**BTA-Passivated Cu NW-Based Capacitive Tactile Sensors.** Transparent, flexible, capacitive tactile sensors were fabricated to demonstrate the potential of BTA-passivated Cu NW networks in optoelectronic device applications. Sensors were used to map the pressure applied by fingers and other objects with various shapes. Figures 6a–c shows the photographs of the fabricated 5 × 5 matrix, single-electrode capacitive sensor devices.

For this capacitive sensor, in the loading mode, only one electrode was used to both transmit and receive signals. Electrodes were loaded capacitively by a conductive object and formed a displacement current flow through a conductive object to the ground. Brining the conductive object closer to the sensor caused an increase in the capacitive coupling between the conductive object and the corresponding electrode. Changes in the magnitude of the output capacitance were proportional to the applied pressure. Figure S7 shows that the output capacitance of the fabricated sensors changes linearly with the applied pressure, where the sensitivity of the sensors was determined as $0.6 \times 10^{-3}$ $\mu$F/kPa. An increase in the applied pressure decreased the thickness of the thermoplastic polyurethane (TPU) layer and increased the capacitance. The capacitance changes of 25 electrodes were recorded as a mapping figure. Figure 6c,f showed an L-shaped conductive object (aluminum foil in this case) that was placed on the device and the corresponding response on the capacitance map, respectively. Contact (touch) information, position, and applied relative pressure of fingers or conductive objects interacting with the device could be obtained through the analysis of the increments in capacitance via mapping figures. As shown in Figure 6d, touching the tactile sensor with three fingers results in different capacitance values ranging from 0.15 to 0.17 $\mu$F.

The fabricated device was also capable of preserving its functionality under bending conditions. Figure 6b shows the photo of the flexible sensor matrix attached to a transparent tube. Upon application of pressure to the sensor surface at three different points, similar and consistent map figures to those for the flat condition were obtained. Lower output capacitance values compared to that of the flat sensor were related to the incomplete coverage of the electrode area by fingers due to the curvature in the bent condition. It is worth noting that the control devices fabricated using bare Cu nanowire networks stopped working only 3 days after production. This signifies the necessity of the use of BTA for protecting these devices.

**CONCLUSIONS**

In summary, a simple, all-solution-based, and highly effective method to improve the resistance of Cu NW networks against oxidation was demonstrated. In this method, bulk Cu
corrosion inhibitor BTA was used for the passivation of Cu NW networks. It was demonstrated that BTA passivation does not affect the optoelectronic performance of networks adversely while providing outstanding oxidation resistance under various mild and harsh environments. Upon exposure to ambient conditions for 1 year, the sheet resistance of BTA-passivated Cu NW networks remained almost constant ($R/R_0 < 1.1$). On the contrary, bare Cu NW networks became nonconductive after only 12 days. Furthermore, BTA-passivated networks exhibited superior stability under long-term exposure to heat and humidity, showing a performance that drastically surpasses that of the bare control sample. In addition, BTA-passivated networks were successfully used as transparent and flexible electrodes for capacitive tactile sensors. Applications of the currently developed BTA-passivated Cu NW networks are not limited to tactile sensors, and they can be used in a wide range of different optoelectronic applications. The results obtained in the current study are of referring significance, as they provide a simple and scalable means to fabricate affordable Cu NW networks with high optoelectronic performance and excellent stability that can be utilized as promising alternatives to existing conventional materials used in optoelectronic devices.

### EXPERIMENTAL SECTION

**Chemicals.** Hexadecylamine (HDA) ($C_{16}H_{33}N$, ≥94.0% (a/a)), copper (II) chloride dihydrate (CuCl2·2H2O, ≥99.0%), (−)-glucose monohydrate (anhydrous, 97.5–102.0%), poly(vinylpyrrolidone) (PVP) (MW = 55 000, monomer-based calculation), benzo triazole (BTA) ($C_6H_5N_3$, ≥99.0%), chloroform (CHCl3, ≥99.8%), and cu lactic acid (90%) were purchased from Sigma-Aldrich and used as received. Poly(3,4-ethylenedioxythiophene)-poly(styrenesulfonate) (PE-DOT:PSS) with pH ~3 was purchased from Heraeus (Heraeus VP Al 4083).

**Synthesis of Cu NWs.** Cu NWs were synthesized according to a previously reported procedure developed by Mohl et al. with slight modifications. In a typical synthesis, 147 mg of CuCl2·2H2O, 350 mg of glucose, 1260 mg of HDA, and 70 mL of deionized (DI) water (18.3 MΩ) were mixed in a glass beaker and stirred for 12 h via vigorous magnetic stirring at room temperature to obtain a homogenous mixture. Afterward, the obtained light blue emulsion was transferred to a Teflon-lined autoclave with 100 mL capacity. The reactor was sealed and heated at 105 °C for 12 h without further stirring. Following synthesis, the NWs were purified by centrifugation and washed repeatedly with DI water and ethanol. Next, a multiphas e separation method was carried out to eliminate the byproducts and to get rid of excess HDA. Following purification, the product was dispersed within a 2 wt % PVP–ethanol solution. Excess PVP was removed by washing the NWs with ethanol. The final product was then dispersed in ethanol for further processing.

**Fabrication and Passivation of Transparent Conducting Electrodes.** Ethanol suspensions of Cu NWs were deposited onto soda lime silica glass and poly(ethylene terephthalate) (PET) substrates using spray coating. Cu NW dispersion was sprayed onto the substrates at 100 °C using an airbrush fed by pure nitrogen gas at 1.5 atm. Following deposition, Cu NW networks on glass were annealed under vacuum at 200 °C for 20 min to get rid of the residual PVP layer and to improve the electrical contact at junctions of Cu NWs. Electrodes on PET were immersed into a lactic acid ethanol solution at a volume ratio of 1:2, which was followed by an ethanol rinse and drying. In the meantime, a 3 wt % BTA–ethanol solution was prepared by stirring at 300 rpm for 10 min in a tightly sealed glass vial at room temperature. The solution was then spin-coated onto Cu NW networks at a speed of 3000 rpm for 30 s after which the samples were dried at 70 °C for 30 min. After 24 h, the samples were rinsed with ethanol to get rid of any excess BTA.

**Fabrication of the Capacitive Tactile Sensor.** For the fabrication of the sensor, BTA-passivated Cu NW networks on PET substrates were used and a 240 μm thick TPU was attached to it as a dielectric layer and mechanical support. Each electrode with a size of 1 × 1 cm² was connected with a load resistor and then a microcontroller unit (MCU). The schematic circuit of the fabricated capacitive sensor for one electrode is shown in Figure S8. The timer inside the MCU calculates the capacitance of the system through elapsed time while pressing.

**Characterizations and Measurements.** SEM was performed with an FEI NOVA NANO SEM 430 operated at 10 kV. Transmission electron microscopy (TEM) images were obtained on a JEOL TEM 2100F operated at 200 kV. X-ray photoelectron spectroscopy (XPS) measurements were performed using SPECS PHOIBOS and PHI 5000 Versa Probe X-ray photoelectron spectrometers with monochromatic Al Kα X-ray excitation sources (15 kV, 400 W, 1486.6 eV) and hemispherical photoelectron energy analyzers. Binding energy (B.E.) calibration was made by setting the adventitious carbon (C 1s) signal to 284.4 eV. Peak fitting, baseline correction, and deconvolution analysis of the XPS data were performed via CASA and OriginPro software. ATR-IR measurements were performed on a Bruker Alpha spectrometer equipped with a Bruker ATR attachment and a DLaTGS detector. Each ATR-IR spectrum was acquired with a frequency resolution of 4 cm⁻¹ by averaging 32 scans. To eliminate atmospheric water and carbon dioxide vibrational signatures, a background spectrum of air was acquired before each sample spectrum.

Sheet resistance and transparency measurements were performed using a Keithley 2400 source meter and an Agilent 8453 UV–vis spectrophotometer, respectively. Continuous humidity and temperature measurements were performed with a chamber-mounted remote Weather Forecast digital hygrometer probe (temperature range = −20 to +50 °C, thermometer accuracy = ±1 °C, humidity range = 20–98% RH, humidity accuracy = ±5%).

### ASSOCIATED CONTENT

#### Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsami.0c11729.

Scanning Electron Microscope (SEM) images, statistical information (diameter and length distribution histograms of nanowires), additional X-ray photoelectron spectroscopy (XPS) results, areal mass density (amd) calculation procedure, and graph related to the tactile sensor capacitance change with respect to pressure (PDF)

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Notes
The authors declare no competing financial interest.

ACKNOWLEDGMENTS
This work was financially supported by the Middle East Technical University through the Scientific Research Projects Programme under project numbers BAP-07-02-2016-003, BAP-07-02-2017-011, and BAP-07-02-2017-004-265. E.O. acknowledges the scientific collaboration with the TARLA project founded by the Ministry of Development of Turkey (project code DPT2006K-120470). The authors also acknowledge Mr. Mete Duman (UNAM, Project code DPT2006K-120470). The authors also acknowledge the financial support of the Middle East Technical University, No. 125202.

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